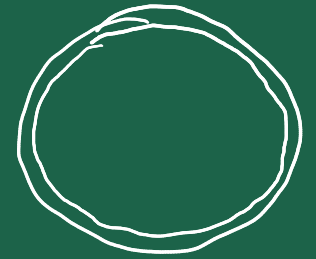


Thick-walled Pressure Vessel

$$t \text{ } \cancel{\times} \text{ } R$$



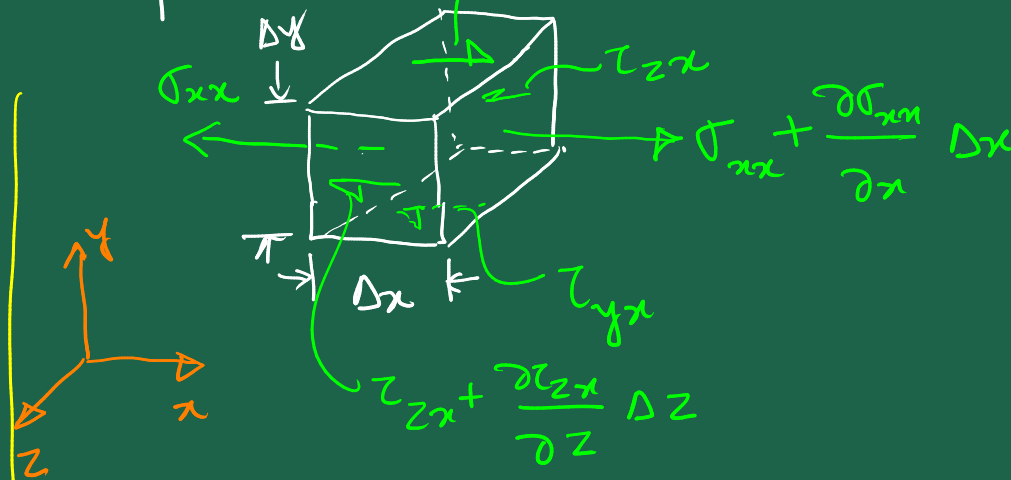
$$\left. \begin{aligned} \sigma_1 &= \frac{p r}{t} \\ \sigma_2 &= \frac{p r}{2t} \end{aligned} \right\} C_y l$$

$$\sigma = \frac{p r}{t} \} s_{ph}$$

$$\rho \frac{\Delta \vec{v}}{\Delta t} = \nabla \cdot \vec{\sigma} + \rho \vec{b}$$

$$\Rightarrow \nabla \cdot \vec{\sigma} = 0$$

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xz}}{\partial z} = 0$$



$$\left(\sigma_{xx} + \frac{\partial \sigma_{xx}}{\partial x} \Delta x \right) - \sigma_{xx} + \left(\tau_{yx} + \frac{\partial \tau_{yx}}{\partial y} \Delta y \right) - \tau_{yx} + \left(\sigma_{zx} + \frac{\partial \sigma_{zx}}{\partial z} \Delta z \right) - \sigma_{zx} = 0$$



$$\sigma_{xx}(x + \Delta x)$$

$$\left(\sigma_{xx} + \frac{\partial \sigma_{xx}}{\partial x} \Delta x\right) - \sigma_{xx} + \left(\tau_{yx} + \frac{\partial \tau_{yx}}{\partial y} \Delta y\right) - \tau_{yx} \\ + \left(\tau_{zx} + \frac{\partial \tau_{zx}}{\partial z} \Delta z\right) - \tau_{zx} = 0$$

$$\Rightarrow \frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z} = 0 \quad (\text{Force balance in } x \text{ dir}^n)$$

Similarly

$$\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} = 0 \quad (\text{" " " } y \text{ "})$$

$$\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} = 0 \quad (\text{" " " } z \text{ "})$$

Stress
eqs.
eqns.



$$\epsilon_{xx} = \frac{\partial u}{\partial x}, \quad \epsilon_{yy} = \frac{\partial v}{\partial y}$$

Stress eqn. eqn in r -dirⁿ

$$\frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r} \left[\frac{\partial \tau_{r\theta}}{\partial \theta} + \sigma_{rr} - \sigma_{\theta\theta} \right] + \frac{\partial \tau_{rz}}{\partial z} = 0$$

3 eqns

6 unknowns
(6 stress comp.)

θ : - - - - -

z : - - - - -

Strain-Displacement } 6 eqns
6 ϵ , 3 $u, v, w \rightarrow$ 9 unknowns

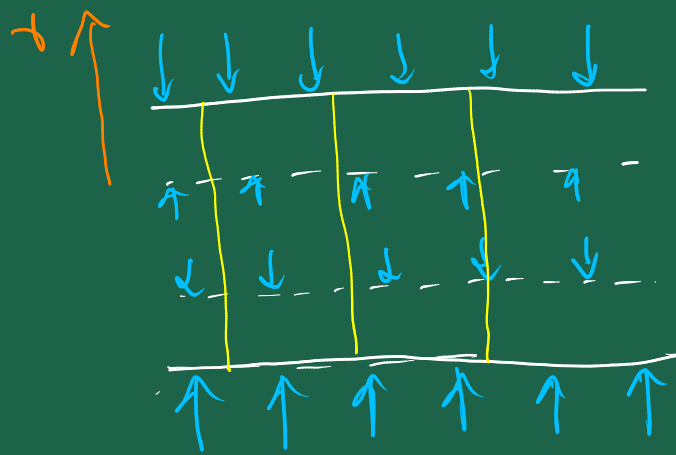
Generalized Hooke's Law } $\rightarrow$ 6 eqns

9 eqns

15 unknowns

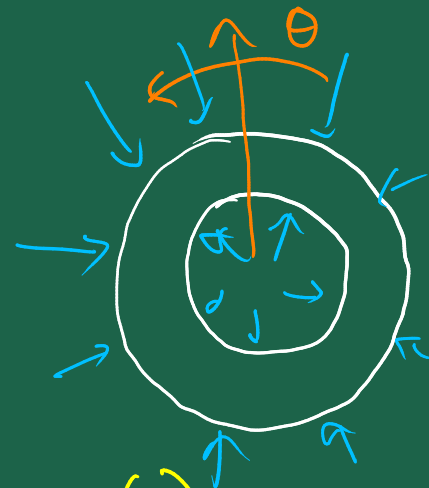
15 eqns

15 unknowns



plane strain $\rightarrow z$

$$\begin{cases} u \equiv u(x, \theta, z) \equiv u(r, \theta) \\ v \equiv v(x, \theta, z) \equiv v(r, \theta) \\ w \equiv w(x, \theta, z) = 0 \end{cases}$$



Axisymmetry : $\frac{\partial}{\partial \theta} \Leftrightarrow$ No θ -dependence $\Rightarrow$

$$\begin{aligned} u &\equiv u(r, \theta) \equiv u(r) \\ v &\equiv v(r, \theta) \equiv v(r) \end{aligned}$$

Loading purely in radial dirⁿ $\Rightarrow v = 0$

$$u \equiv u(r), \quad v = 0, \quad w = 0$$

Plane strain: $\epsilon_{zz} = 0$, $\epsilon_{z\theta} = 0$, $\epsilon_{zr} = 0$

$$\Rightarrow \tau_{zr} = 2G\epsilon_{zr} = 0$$

Stress eqn. eqn in r -dirⁿ

$$\frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r} \left[\underbrace{\frac{\partial \tau_{r\theta}}{\partial \theta}}_{=0} + \sigma_{rr} - \sigma_{\theta\theta} \right] + \frac{\cancel{\tau_{rz}}}{\partial z} = 0$$

$$\Rightarrow \boxed{\frac{\partial \sigma_{rr}}{\partial r} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} = 0}$$

$$\cancel{0} \leftarrow \epsilon_{zz} = \frac{1}{E} \left[\sigma_{zz} - \nu(\sigma_{rr} + \sigma_{\theta\theta}) \right] \Rightarrow \sigma_{zz} = \nu(\sigma_{rr} + \sigma_{\theta\theta})$$

$$\begin{aligned}
 \epsilon_{rr} &= \frac{1}{E} [\sigma_{rr} - \nu(\sigma_{\theta\theta} + \sigma_{zz})] \leftarrow \sigma_{zz} = E(\epsilon_{rr} + \epsilon_{\theta\theta}) \\
 \epsilon_{\theta\theta} &= \frac{1}{E} [\sigma_{\theta\theta} - \nu(\sigma_{rr} + \sigma_{zz})] \leftarrow \\
 \epsilon_{rr} &= \frac{1+\nu}{E} [(1-\nu)\sigma_{rr} - \nu\sigma_{\theta\theta}] \rightarrow \begin{aligned} \sigma_{rr} &= \frac{E}{(1+\nu)(1-2\nu)} [(1-\nu)\epsilon_{rr} + \nu\epsilon_{\theta\theta}] \\ \sigma_{\theta\theta} &= \frac{E}{(1+\nu)(1-2\nu)} [(1-\nu)\epsilon_{\theta\theta} + \nu\epsilon_{rr}] \end{aligned} \\
 \epsilon_{\theta\theta} &= \frac{1+\nu}{E} [(1-\nu)\sigma_{\theta\theta} - \nu\sigma_{rr}] \rightarrow
 \end{aligned}$$

Now, we use the strain-displacement relations (simplified)

$$u = u(r)$$

$$\epsilon_{rr} = \frac{du}{dr}, \quad \epsilon_{\theta\theta} = \frac{u}{r}$$

$$\sigma_{rr} = \frac{E}{(1+\nu)(1-2\nu)} \left[(1-\nu) \frac{du}{dr} + \nu \frac{u}{r} \right]$$

$$\sigma_{\theta\theta} = \frac{E}{(1+\nu)(1-2\nu)} \left[(1-\nu) \frac{u}{r} + \nu \frac{du}{dr} \right]$$

e^{mx}

$$\rightarrow \frac{\partial \sigma_{rr}}{\partial r} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} = 0$$

$$\Rightarrow \boxed{\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} - \frac{u}{r^2} = 0}$$

← 2nd order, linear
diff. eqn
(ODE)

$$\frac{du}{dr} \frac{du}{dr} \times$$

$$u \frac{du}{dr} \times$$

$$u = r^m$$

$$\rightarrow m(m-1)r^{m-2} + m r^{m-2} - r^{m-2} = 0$$

$$m(m-1)r^{m-2} + m r^{m-2} - r^{m-2} = 0$$

$$\Rightarrow m(m-1) + m - 1 = 0$$

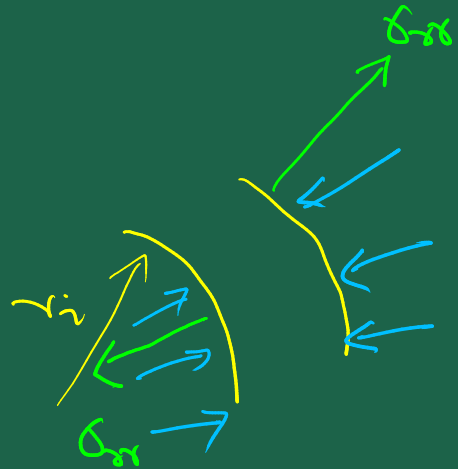
$$\Rightarrow m^2 - 1 = 0$$

$$\Rightarrow m = \pm 1$$

$$u = A_1 r^1 + A_2 r^{-1} \Rightarrow u = A_1 r + \frac{A_2}{r}$$

For the B.C.s reqd to solve for A_1 and A_2 ,

$$\sigma_{rr} \big|_{r=r_i} = -p_i \quad ; \quad \sigma_{rr} \big|_{r=r_o} = -p_o$$



$$-p_i^{\check{r}} = \frac{E}{(1+\check{\nu})(1-2\check{\nu})} \left[A_1 - (1-2\check{\nu}) \frac{A_2}{r_i^2} \right]$$

$$-p_o^{\check{r}} = \frac{E}{(1+\check{\nu})(1-2\check{\nu})} \left[A_1 + \underline{(1-2\check{\nu})} \frac{A_2}{r_o^2} \right]$$

Find A_1 and A_2

$$\sigma_{rr} = C_1 - \frac{C_2}{r^2}, \quad \sigma_{\theta\theta} = C_1 + \frac{C_2}{r^2}$$

where

$$C_1 = \frac{p_i r_i^2 - p_o r_o^2}{r_o^2 - r_i^2}, \quad C_2 = \frac{(p_i - p_o) r_i^2 r_o^2}{r_o^2 - r_i^2}$$

$$\rightarrow \sigma_{rr} + \sigma_{\theta\theta} = 2C_1 \\ = \text{const.}$$

$$\sigma_{zz} = \check{\nu} (\sigma_{rr} + \sigma_{\theta\theta}) \\ = \text{const.}$$